



STATE ATOMIC ENERGY CORPORATION "ROSATOM"

STRAIN RATE INFLUENCE ON DYNAMIC PROPERTIES OF STEEL U10A

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Mechanical properties of steel U10A

Material	Hardness	σ_B , kgf/mm ²	$\sigma_{0.2}$, kgf/mm ²	δ , %	$\sigma_{сж}$, kgf/mm ²	Note
Steel U10A	197HB	55-65	22-35	55	440-480	
Quenched steel U10A	65HRC	172	-	-	530-540	heating 770-780°C tempering 140-160 °C

The goal of this work:

-to investigate the influence of strain rate on the strength properties of steel U10A in as-received state and after quenching to use it for selecting the parameters of Johnson-Cook model with Mie-Gruneisen equation.

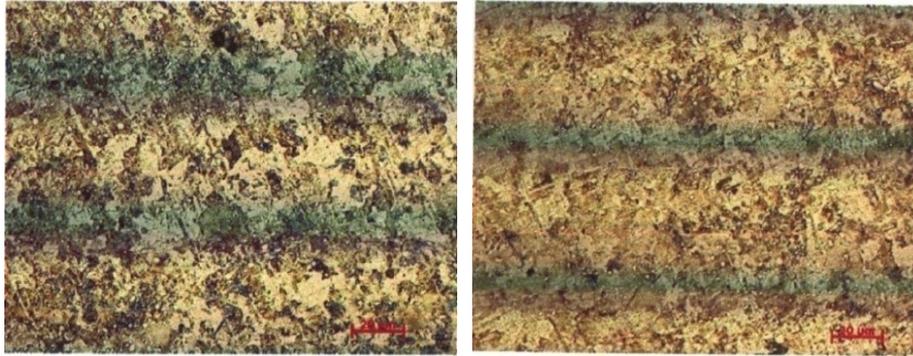
$$Y = (A + B\varepsilon_p^n) \cdot \left(1 + c \ln \frac{\dot{\varepsilon}_p}{\dot{\varepsilon}_0} \right) \cdot \left(1 - \left[\frac{T - T_r}{T_m - T_r} \right]^m \right)$$

$$P = \frac{\rho_0 C_0^2 \mu \left[1 + \left(1 - \frac{\gamma_0}{2} \right) \mu - \frac{a}{2} \mu^2 \right]}{\left[1 - (S_1 - 1) \mu - S_2 \frac{\mu^2}{\mu + 1} - S_3 \frac{\mu^3}{(\mu + 1)^2} \right]} + (\gamma_0 + a \mu) E$$

Johnson, G.R. and W.H. Cook, .A Constitutive Model and Data for Metals Subjected to Large Strains, High Strain Rates and High Temperatures. Presented at the Seventh International Symposium on Ballistics, The Hague, The Netherlands, April 1983.

Chemical composition of steels U10A (GOST 1435-99)

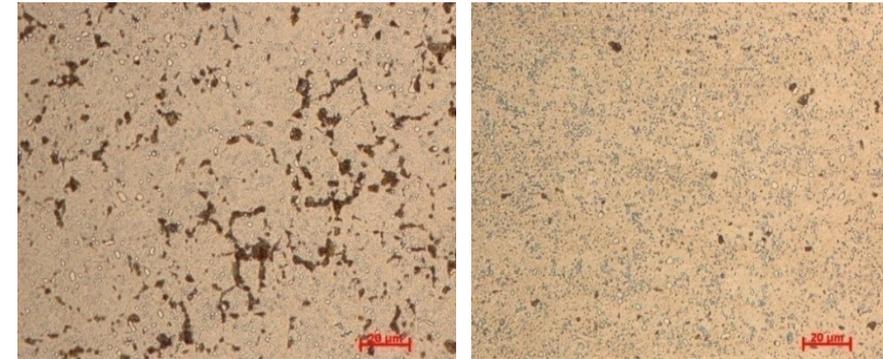
Steel grade	mass share element, %							
	Carbon	Silicon	Manganese	Sulfur	Phosphorus	Chrome	Nickel	Copper
	not more than							
U8A	0,75-0,85	0,17-0,33	0,17-0,28	0,018	0,025	0,12	0,12	0,2
U10A	0,95-1,09	0,17-0,33	0,17-0,28	0,018	0,025	0,12	0,12	0,2
U12A	1,16-1,23	0,17-0,33	0,17-0,28	0,018	0,025	0,12	0,12	0,2



Micro structure of transverse (left) and longitudinal (right) sections of the sample in initial state (group I).

Magnification $\times 500$

Lamellar perlite



Micro structure of transverse (left) and longitudinal (right) sections of the sample after quenching (group Z)

Magnification $\times 500$

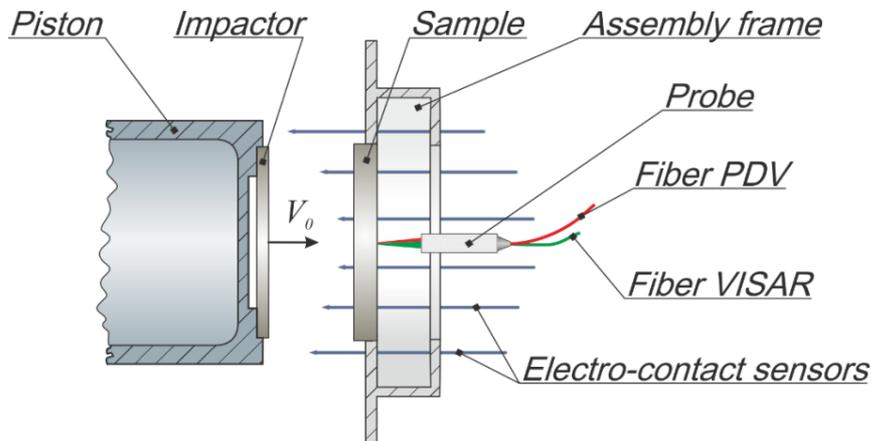
Granular perlite

Properties of steel U10A samples under study

Material	ρ , g/cm ³	HV _{0,1} gf/mm ²	C_p , m/s	C_s , m/s	C_θ , m/s	E , MPa	G , MPa	K , MPa
Steel U10A in initial state (group I)	7,77	429-775	5977	3229	4671	209,6	81	169,6
Quenched steel U10A (group Z)	7,77	856- 916	6654	3590	5205	259,3	100,1	201,5

As the result of quenching, the structure of steel U10A changed from lamellar perlite to granular perlite, Shear modulus G of steel U10A increased by 19%, Young modulus E compression modulus K – by 22..23%.

Experimental equipment



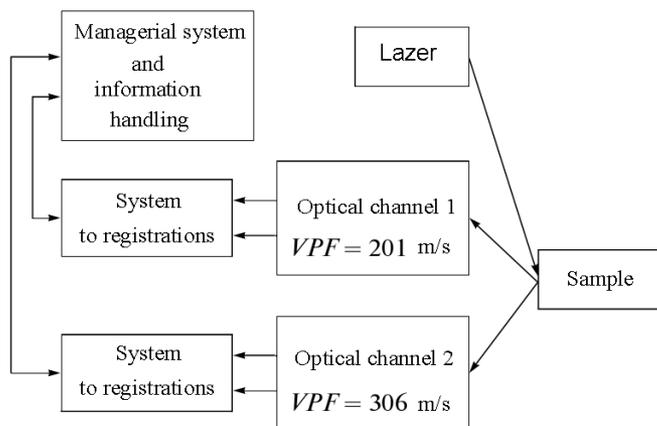
Registration of velocity $W(t)$:

- VISAR
- PDV

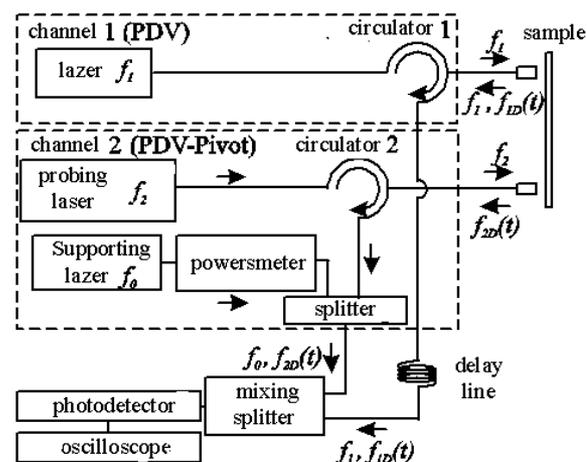
Impact velocity V_0 :

- ECS

VISAR system



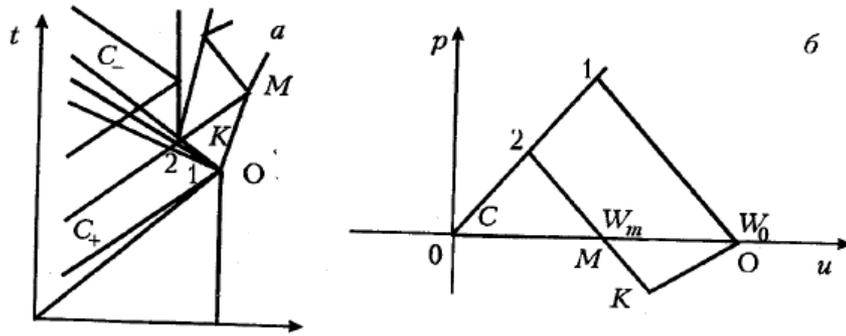
PDV system



A.V. Pavlenko, S.I. Balabin, O.E. Kozelkov, D.N. Kazakov. One-step light-gas gun for investigation into dynamic properties of structural materials in the range up to 40 GPa // priory i tekhnika eksperimenta, 2013, №4, C.122-124.

S.N. Malyugina, V.V. Pereshitov, I.N. Lisitsyna. Two-channel interferometric complex VISAR for investigation into material properties under shock-wave loading // priory i tekhnika eksperimenta, 2013, #2, p.127-129.

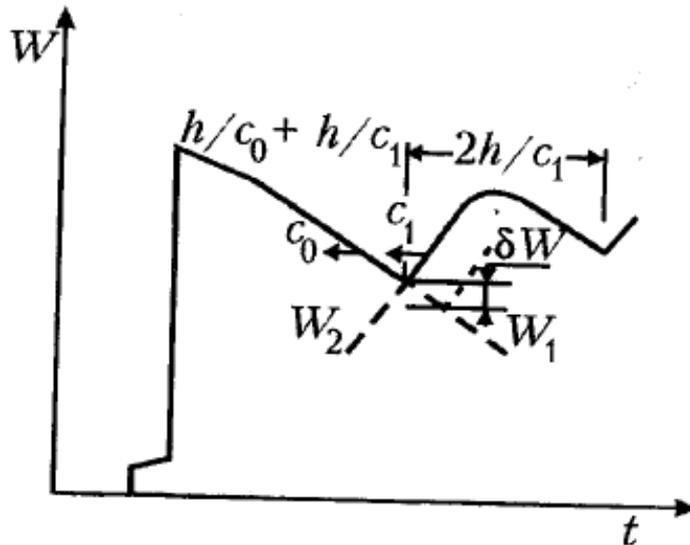
S.S. Mokrushin, N.B. Anikin, S.N. Malyugina, A.V. Pavlenko, A.A. Tyaktev. Interferometer with frequency-time multiplexing for investigation into material properties in shock-wave experiments // priory i tekhnika eksperimenta, 2013, #4, p.107-109.



$$\sigma_{sp} = 0,5 \cdot \rho_0 \cdot C_0 \cdot (W_0 - W_m + \delta W)$$

$$\delta W = \left(h/c_0 - h/c_1 \right) \cdot \frac{|\dot{W}_1 \cdot \dot{W}_2|}{|\dot{W}_1| + \dot{W}_2}$$

$$\frac{\dot{V}}{V_0} = \frac{\dot{W}}{2C_0}$$



$$\sigma_{hel} = 0.5 \cdot \rho_0 \cdot c_1 \cdot W_{hel}$$

$$\sigma_{\tau} = 1.5 \cdot \sigma_{hel} \cdot \left(1 - c_0^2/c_1^2 \right)$$

$$\tau_T = 0.75 \sigma_{hel} \left(1 - c_0^2/c_1^2 \right)$$

Data on experiment set-up

Data on experiment set-up with samples of steel U 10A in initial state (group I)

Date and # of experiment	Impact or thickness h_y , mm	Velocity V_0 , m/s	Mismatch, mrad	Sample thickness h_0 , mm
#106 of 23.10.15	1.986	809.2±2.4	1.9	4.001
#107 of 26.10.15	1.989	626.9±1.9	0.37	3.998
#108 of 27.10.15	1.983	397.2±2.0	0.78	3.998
#109 of 28.10.15	1.984	197.1±0.6	0.65	3.998
#113 of 05.11.15	1.991	171±2	-	4.003
#114 of 06.11.15	1.984	751.8±2.3	2.3	3.994
#115 of 10.11.15	1.991	1027.9±3.1	0.47	4.005
#116 of 12.11.15	1.004	651.7±2	0.91	1.983
#117 of 13.11.15	0.464	667.7±2.0	1.16	1.024
#118 of 16.11.15	1.983	639.7±1.9	2.45	7.981
#119* of 18.11.15	0.091	629.0±4.4	0.51	0.577
#120 of 20.11.15	0.472	416.5±0.8	0.90	1.007
#126 of 30.11.15	2.015	342.3±0.7	0.46	3.989

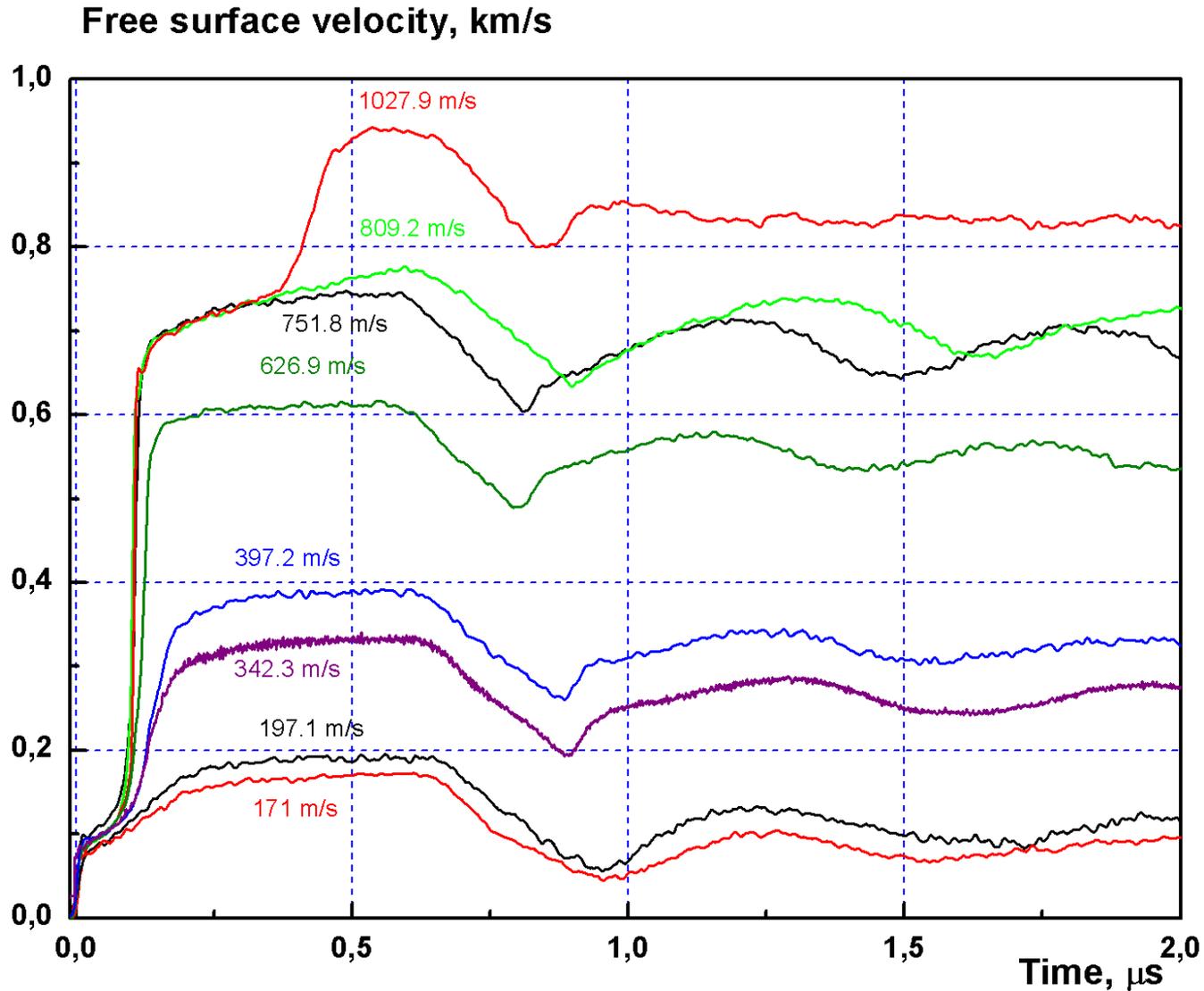
In all experiments, steel U10A was used in initial state for impactors and samples

* foil out of steel 12Kh18N10T was used for impactor

Data on experiment set-up with samples of quenched steel U 10A (group Z)

Date and # of experiment	Impactor thickness h_y , mm	Velocity V_0 , m/s	Mismatch, mrad	Sample thickness h_0 , mm
#133OT 10.12.15	1.912	393.4±1.2	0.85	3.941
#135 OT 14.12.15	1.908	987.5±2.9	0.98	3.949
#137*OT 18.12.15	0.51	409.6±0.8	0.28	0.868
In all experiments, steel U10A was used in quenched state for impactors and samples * impactor – steel 30KhGSA				

Experimental profiles of free surface velocity for steel U10A in initial state (group I). $V_0=171-1027.9$ m/s 2/4 mm.



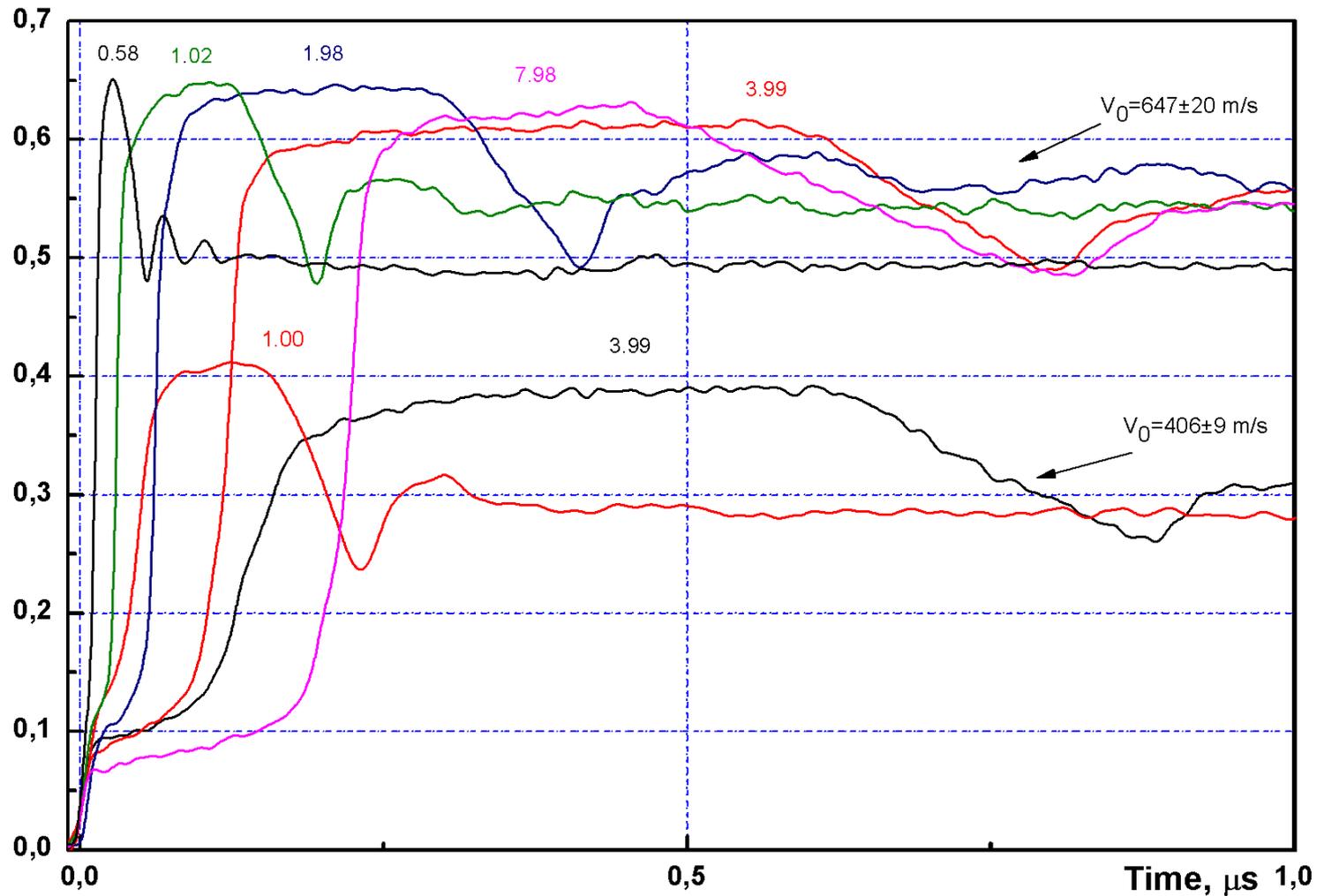
Experimental profiles of free surface velocity

For steel U10A in initial state (group I).

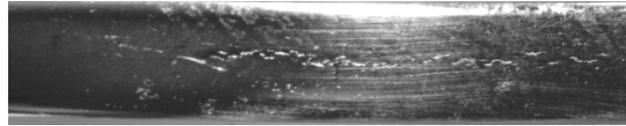
$V_0 = 647 \pm 20$ m/s and $V_0 = 406 \pm 9$ m/s.



Free surface velocity, km/s

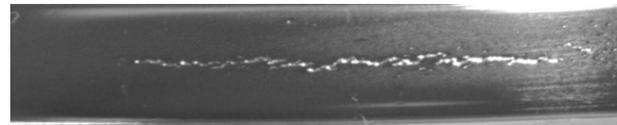


Experiments with samples of steel U10A in initial state (group I)



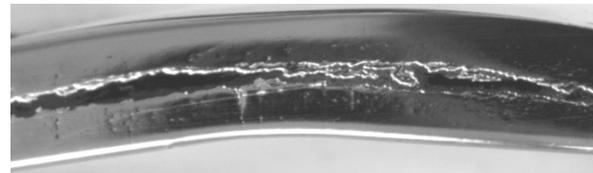
Intensive micro destruction
In the form of separate cracks

Experiment #113 ($\tau=0,85 \mu\text{s}$; $V_0= 171\pm 2,0 \text{ m/s}$)



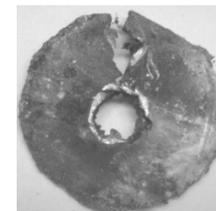
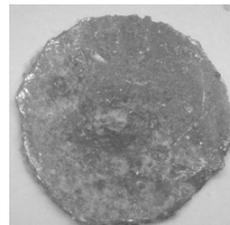
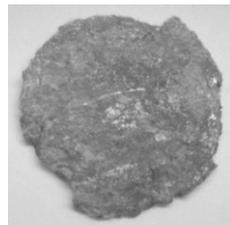
Weak macro destruction,
“forming” region of
spallation destruction

Experiment #109 ($\tau=0,82 \mu\text{s}$; $V_0= 197,1\pm 0,6 \text{ m/s}$)



Partial spallation destruction
in the form of main crack

Experiment #108 ($\tau=0,75 \mu\text{s}$; $V_0= 397,2\pm 2,0 \text{ m/s}$)



Complete spallation
destruction,
Thickness of
spallation layers
1,8..2,2 mm

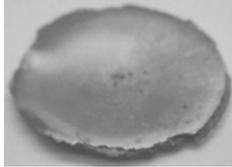
Experiment #107
 $\tau=0,68 \mu\text{s}$,
 $V_0= 626,9\pm 1,9 \text{ m/s}$

Experiment #114
 $\tau=0,71 \mu\text{s}$,
 $V_0= 751,8\pm 2,3 \text{ m/s}$

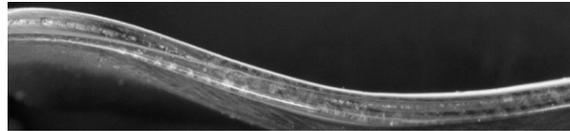
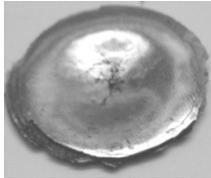
Experiment #106
 $\tau=0,8 \mu\text{s}$,
 $V_0=809,2\pm 2,4 \text{ m/s}$

Experiment #115
 $\tau=0,75 \mu\text{s}$,
 $V_0= 1027,9\pm 3,1 \text{ m/s}$

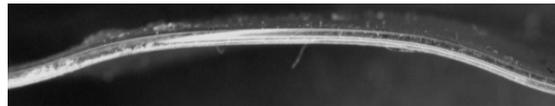
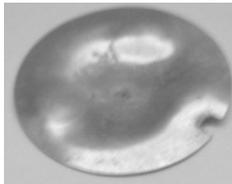
Experiments with samples of steel U10A in initial state (group I) at various duration of loading



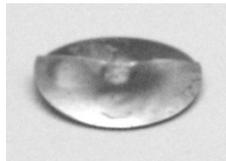
Experiment #116 ($\tau=0,35 \mu\text{s}$, $V_0=651,7\pm 2 \text{ m/s}$)



Experiment #117 ($\tau=0,15 \mu\text{s}$, $V_0=667,7\pm 2,0 \text{ m/s}$)

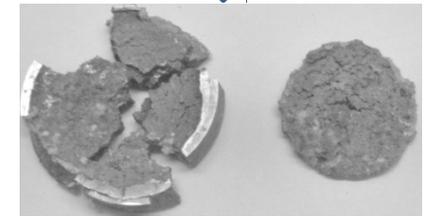


Experiment # 119 ($\tau= 0,04 \mu\text{s}$, $V_0 = 629,0\pm 4,4$)



Experiment #120 ($\tau= 0,18 \mu\text{s}$, $V_0=416,5\pm 0,8$)

Complete destruction like
in experiment # 107
at $V_0= 626,9\pm 1,9 \text{ m/s}$



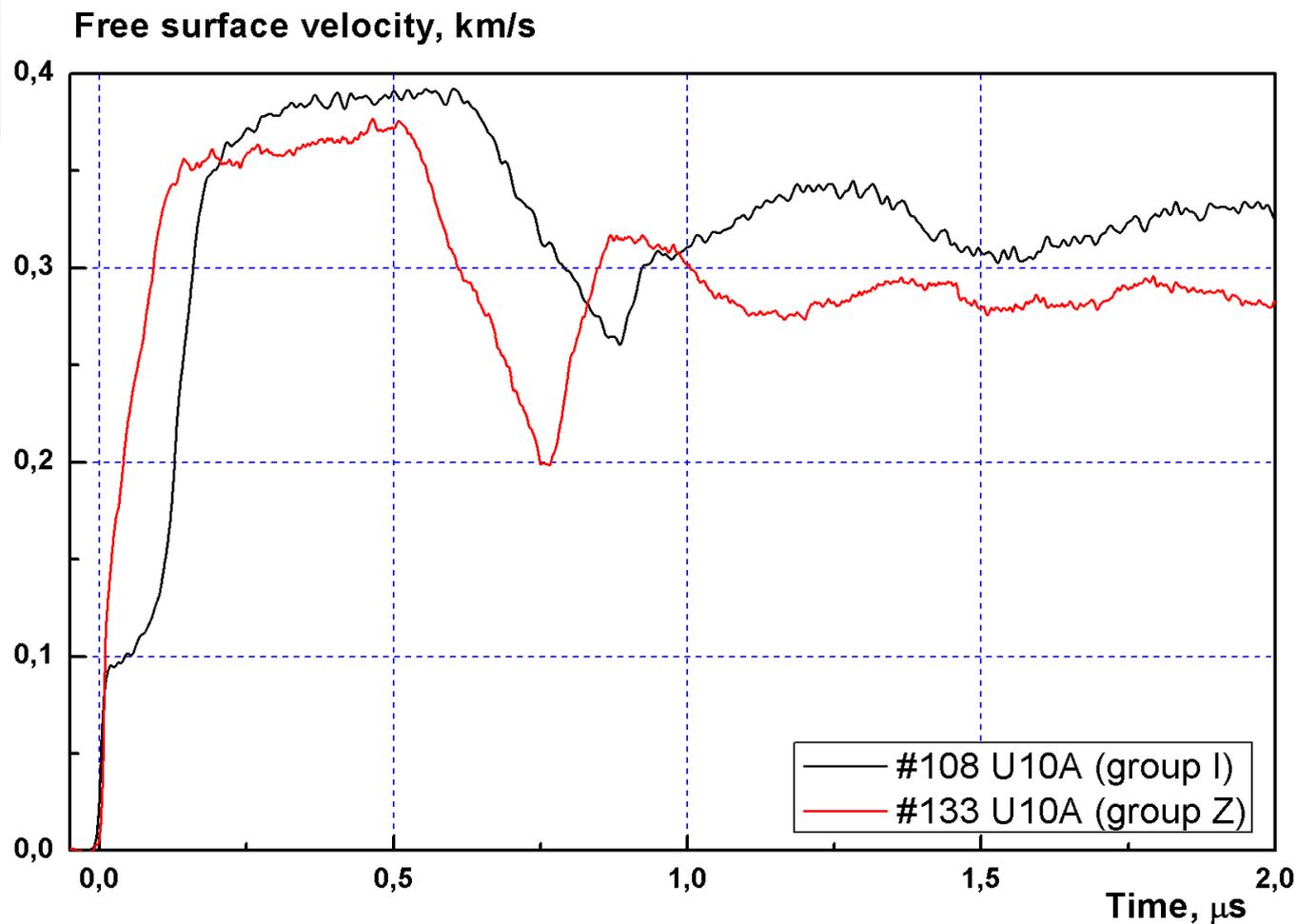
Experiment #118
($\tau= 0,59 \mu\text{s}$, $V_0 = 639,7\pm 1,9$)



Experiment #107
 $\tau=0,68 \mu\text{s}$,
 $V_0= 626,9\pm 1,9 \text{ m/s}$

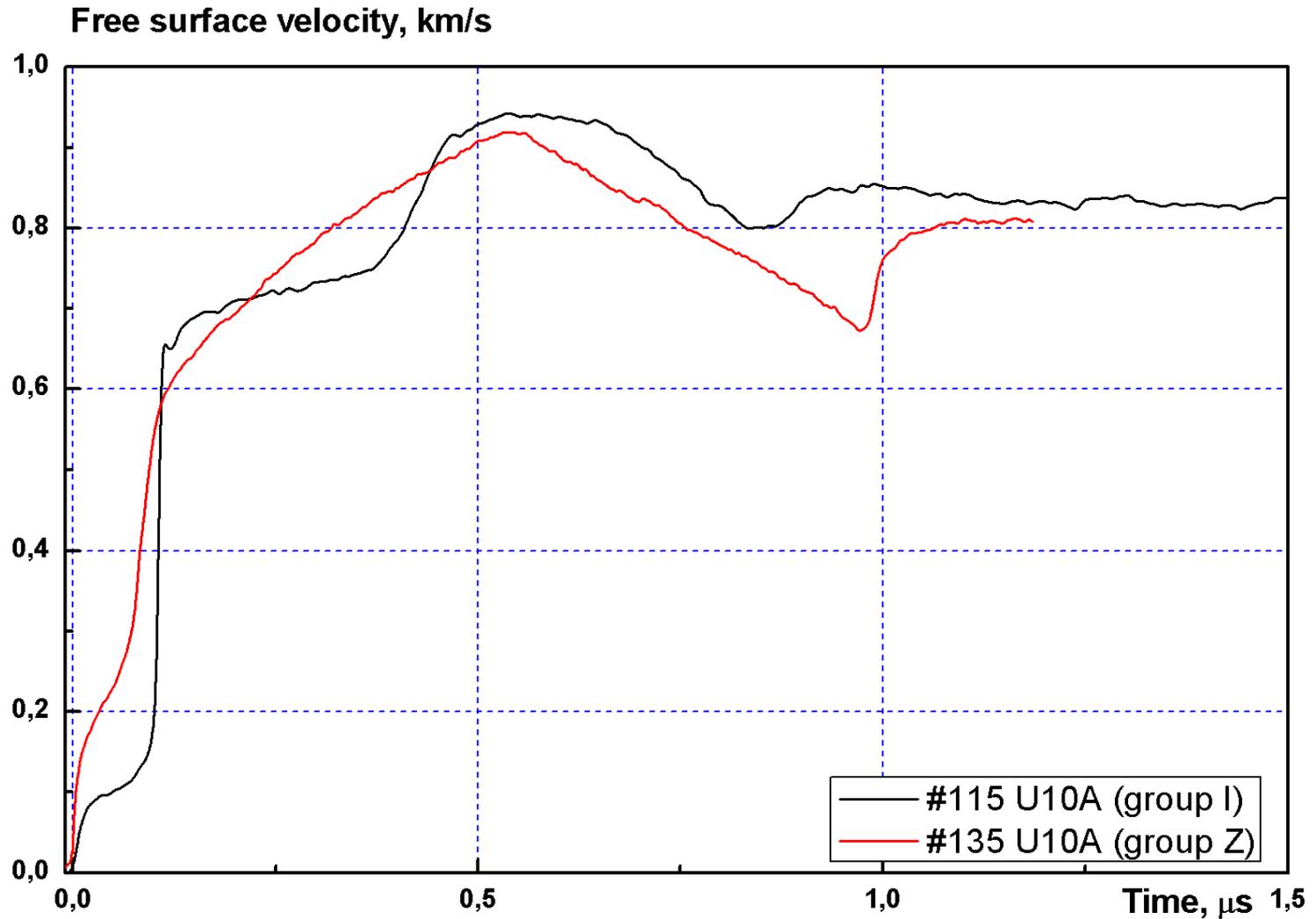
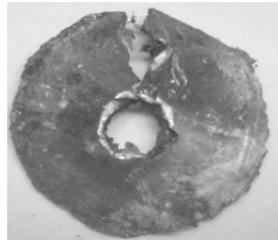
It is seen that with decrease of shock-wave loading, the character of destruction changes, and the samples are destroyed partially. In order to have more detailed information, it is necessary to conduct metallographic analysis.

Experiments with the samples
out of quenched steel U10A
Compared velocity profiles $W(t)$ for both groups of steel U10A.
Experiments #108 and #133 ($V_0 \sim 400$ m/s, 2/4 mm)



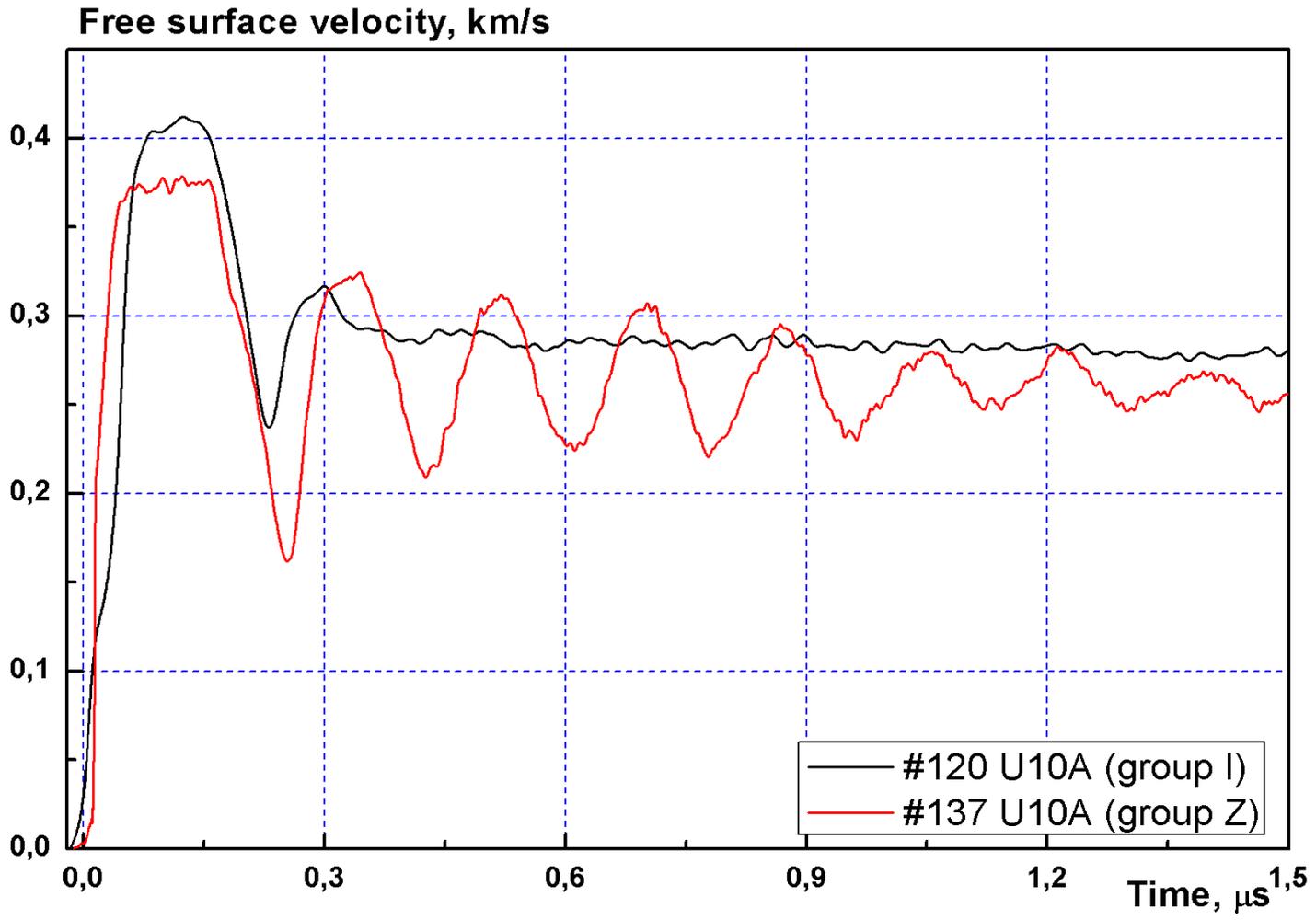
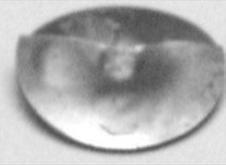
Compared profiles of velocity $W(t)$ for both groups of steel U10A samples.

Experiments #115 and #135 ($V_0 \sim 1$ km/s, 2/4 mm)

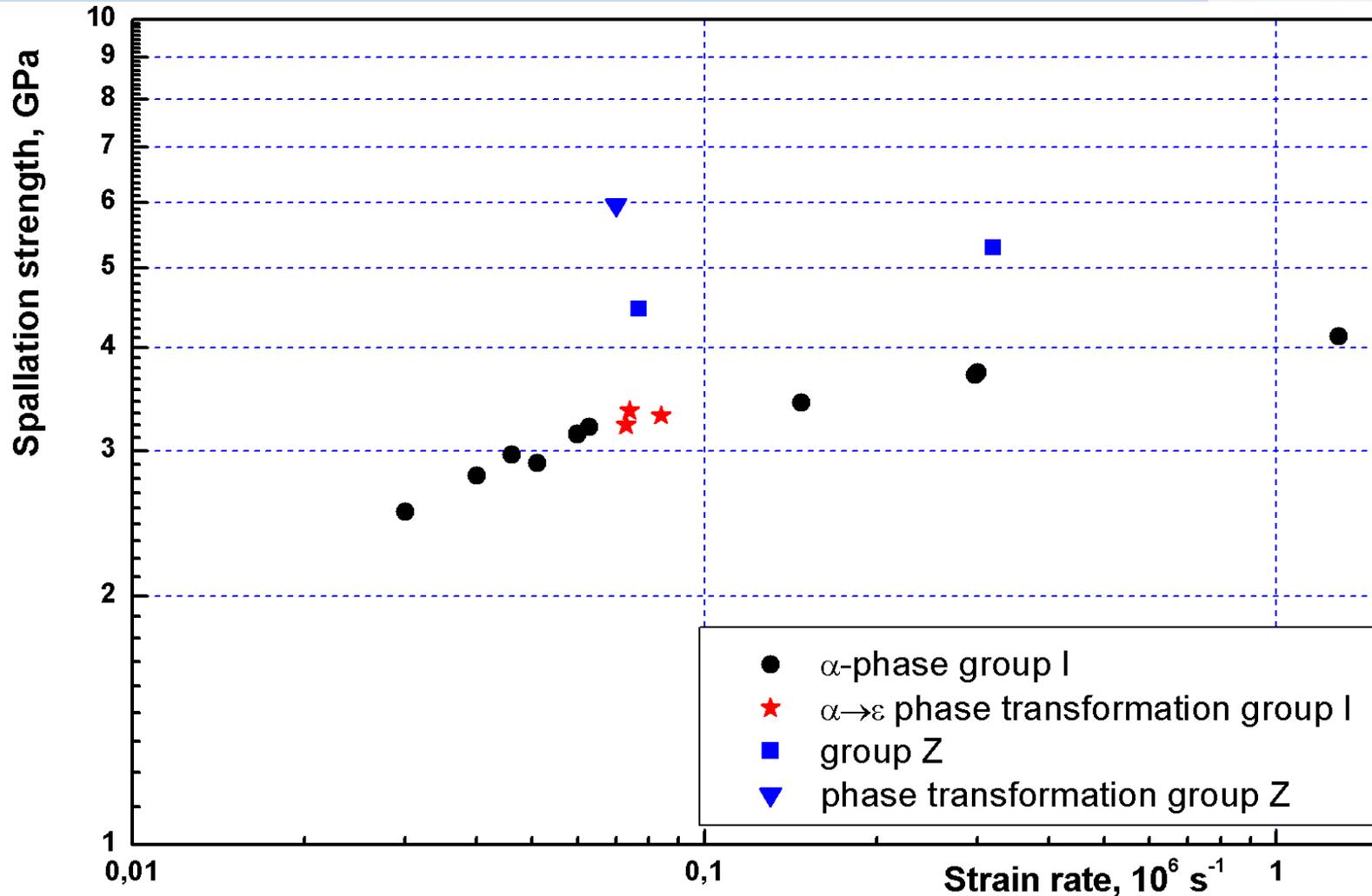


Compared profiles of velocity $W(t)$ for both groups of steel U10A samples.

Experiments #120 and #137 ($V_0 \sim 400$ m/s, 0.5/1 mm)

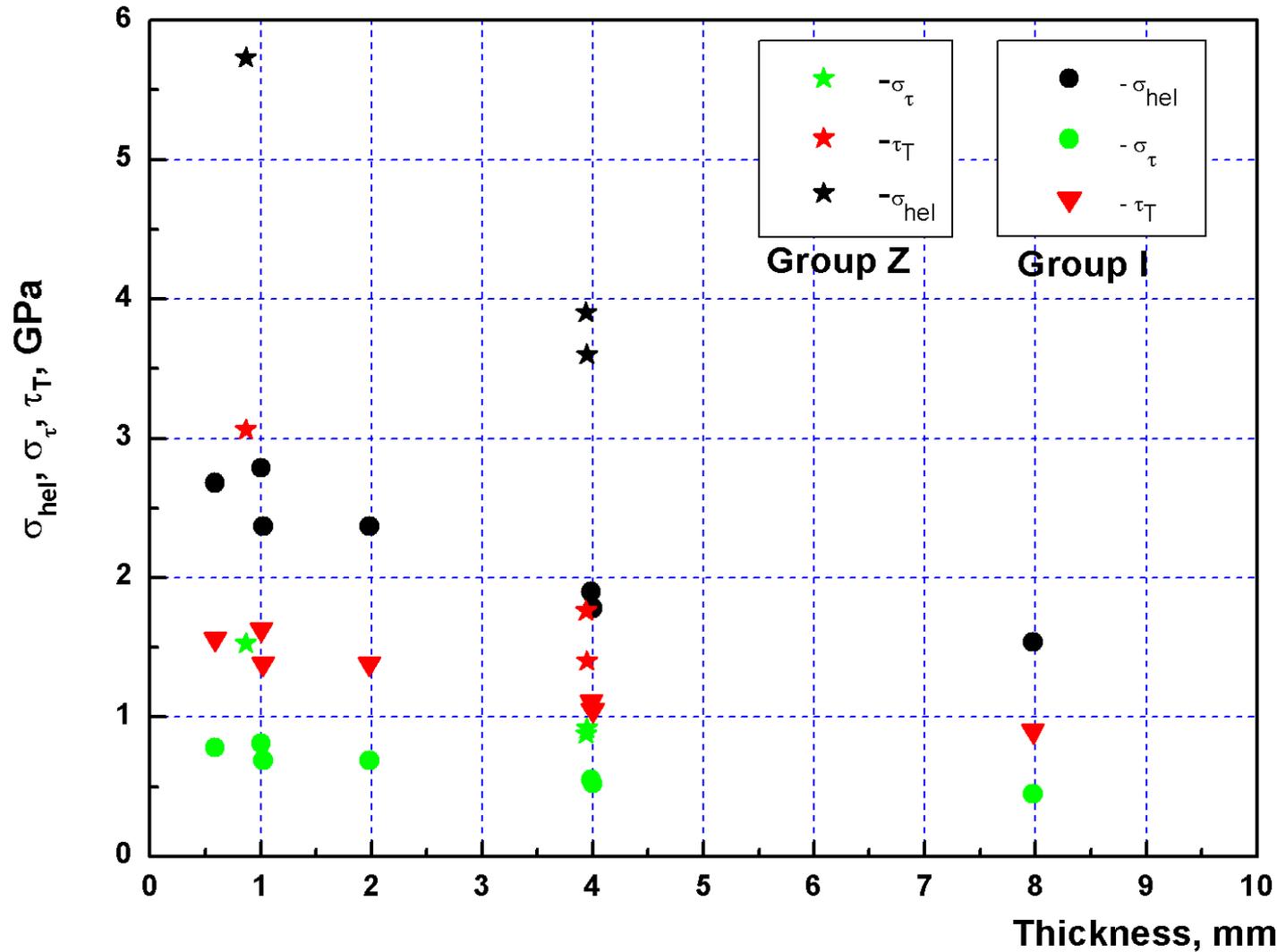


Dependences of spallation strength on strain rate for both groups of steel U10A



The value σ_{sp} for samples of steel U10A (group I) that were subjected to phase transformation was in the range 3,2..3,4 GPa, while the value for the sample out of quenched steel U10A that was subjected to phase transformation was $\sigma_{sp}=5,95$ GPa. In experiments #133 and 137 $\sigma_{sp}=4,45$ Gpa and $\sigma_{sp}=5,28$ GPa.

Dependences σ_{hel} , σ_{τ} and τ_{τ} on thickness for both groups of steel U10A samples



In experiments for the samples with the thickness 4 mm, the values σ_{hel} increased from 1,7... 1,9 GPa up to 3,6... 3,9 GPa, and for the samples with the thickness 1 mm – from 2,7...2,8 up to 5,7 GPa. The values of dynamic yield limit σ_{τ} and shear stress τ_{τ} also increased. For the samples with the thickness 1 mm, the values σ_{τ} increased from 1,4...1,6 up to 3,1 GPa and τ_{τ} – from 0,8 up to 1,6 GPa, and for the samples with the thickness 4 mm – σ_{τ} from 1,1 up to 1,8 GPa and τ_{τ} cfrom 0,5 up to 0,9 Gpa.

CONCLUSION

In experimental physics division, on single-stage light-gas gun LGP-1200, we conducted shock-wave experiments on investigation into dynamic properties of steel U10A samples in initial state and after quenching.

The goal of investigation was to determine unknown dynamic properties of carbon steel U10A and to use experimental profiles of sample free surface velocity for selecting the parameters of Johnson-Cook model with Mie-Gruneisen equation of state.

According to the results of investigation into dynamic properties of steel U10A in initial state (group I), it is possible to make the following conclusions:

- in initial state, the material has tendency to harden in the range of strain rate from $0,03 \cdot 10^6$ up to $1,3 \cdot 10^6 \text{ s}^{-1}$;
- in the process of shock wave propagation, dynamic elastic strength σ_{hel} monotonously decreases from 2,8 GPa at a distance 0,5 mm up to 1,6 GPa at a distance 8 mm;
- dynamic yield limit decreases from σ_{τ} decreases from 1,63 GPa up to 0,9 GPa;
- shear stress τ_{τ} decreases from 0,9 GPa up to 0,47 GPa.

The comparison of the results of dynamic properties measurement for the samples out of quenched steel U10A and the same steel in initial state shows that:

- quenched steel U10A has 1,35..1,4 times higher value of spallation strength;
- dynamic elastic strength σ_{hel} , yield limit σ_{τ} and shear stress τ_{τ} increased in quenched steel U10A, namely: in experiments with the samples 4 mm thick, the values σ_{hel} increased from 1,7... 1,9 GPa up to 3,6... 3,9 GPa, and with the samples 1 mm thick – from 2,7...2,8 up to 5,7 GPa. For the samples 1 mm thick, the values σ_{τ} increased from 1,4... 1,6 up to 3,1 GPa and τ_{τ} – from 0,8 up to 1,6 GPa, and for the samples 4 mm thick, σ_{τ} increased from 1,1 up to 1,8 GPa and τ_{τ} increased from 0,5 up to 0,9 GPa, respectively.
- dynamic elastic strength σ_{hel} , yield limit σ_{τ} and shear stress τ_{τ} also monotonously decrease, as far as the thickness of the samples increases.

**THANK YOU FOR YOUR
ATTENTION !**