



Thermal Responses of PBX-6 Explosives Components

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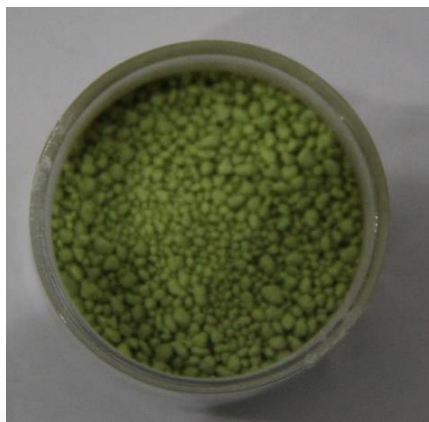
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The thermal sensitivity and safety of explosive and its component have been paid attention to by domestic and abroad researchers, and the corresponding methods of experiment and evaluation are established.

2 Experimental

2.1 Preparation of samples



(a) modeling powder



(b) explosive cylinder

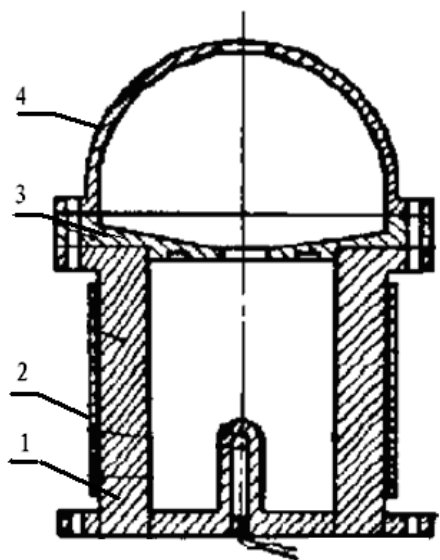


(c) half sphere

Fig.1 Explosive samples of different sizes



2.2 Method of explosion point test



5s delay explosion temperature(T_{5s})

1000s critical temperature(T_{1000s})

Fig.2 Scheme of explosion point test setup



2.3 Method of thermal explosion test

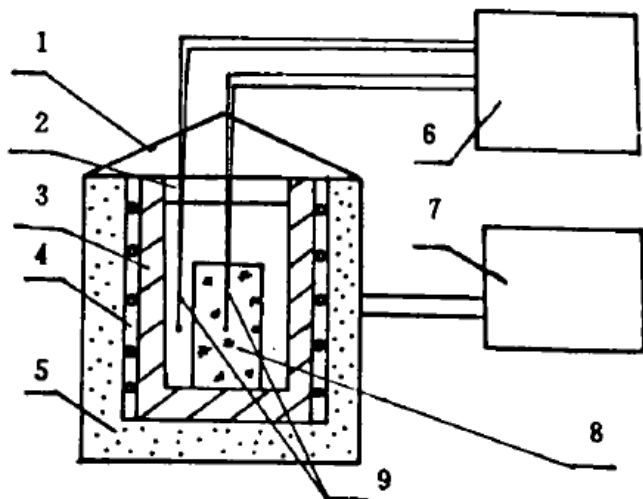


Fig.3 Scheme of Unlimited thermal explosion test setup

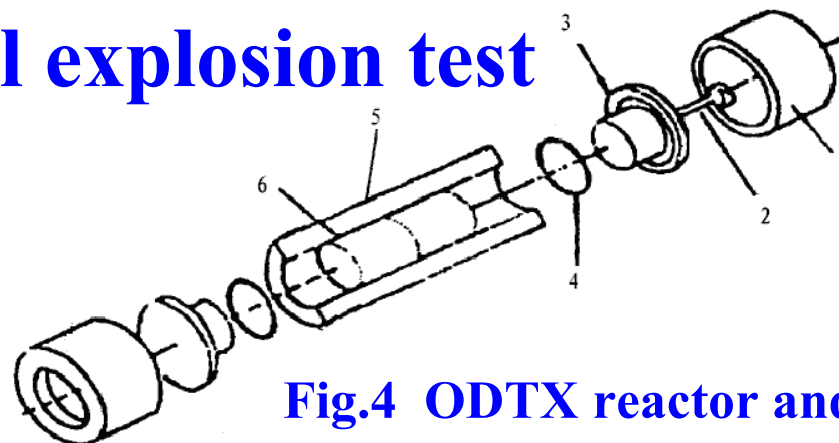


Fig.4 ODTX reactor and sample assembly sketch

one dimension time-to-explosive test is one of standard method to evaluate the safety of explosive component in U.S.A

critical temperature (T_m)
delay time (t)

U.S.A
two $\Phi 0.5 \times 1$ inch

China
two $\Phi 13 \times 26$ mm



**destruction degree
of sample reactor**

- (a) non-reaction**
- (b) middle pressure release**
- (c) low level reaction**
- (d) high level reaction**

Fig.5 Evaluated method of reaction grades in ODTX test



2.4 Method of cook-off test

bonfire stimulation

slow heating stimulation



Fig.6 Photograph of fast cook-off test for explosive component



Fig.7 Photograph of slow cook-off test setup of encased thermocouples and explosive components

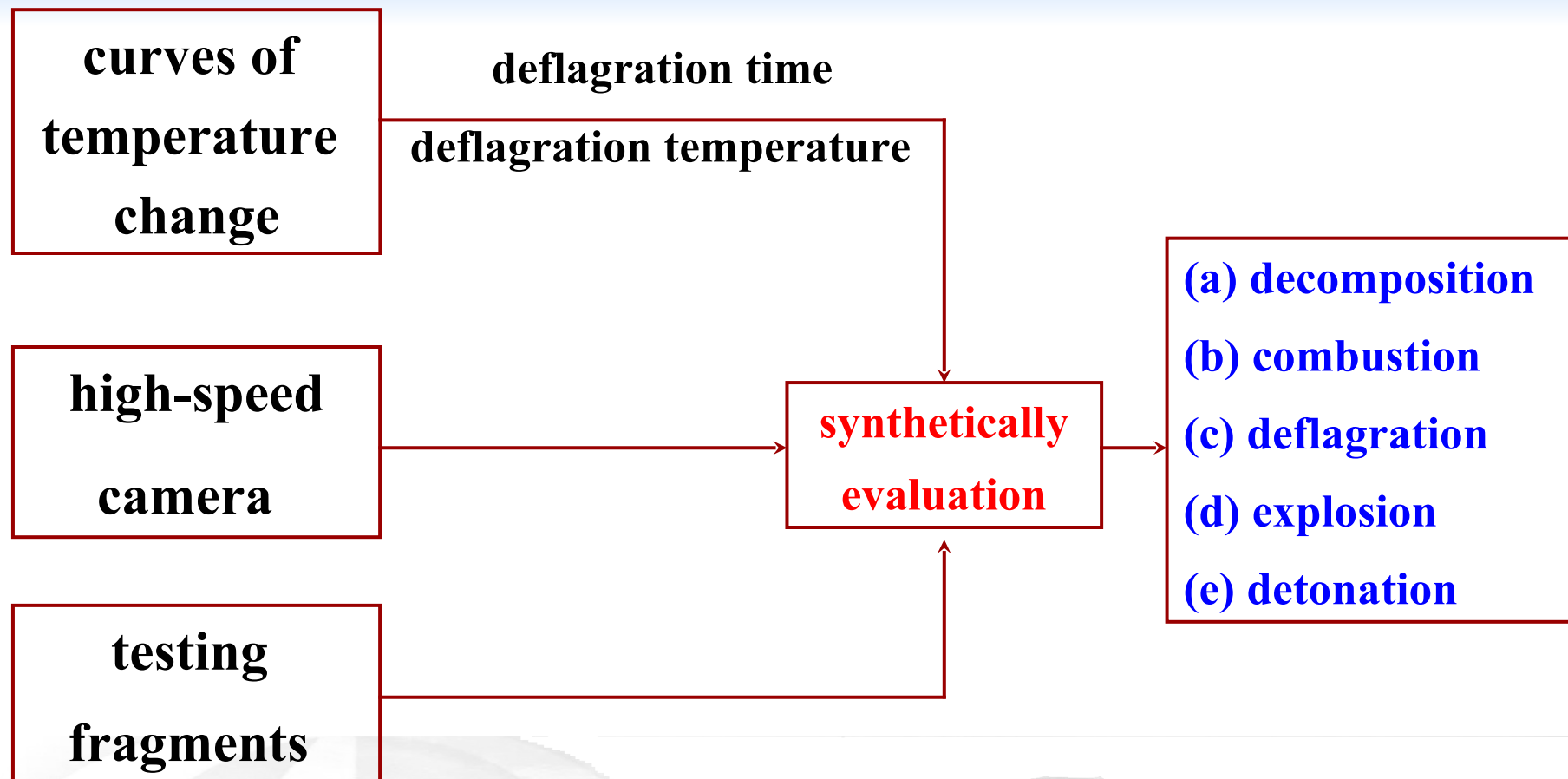


Fig.8 Evaluated method of reaction grades in cook-off test



3.1 Explosion points of small-scale explosive

The thermal sensitivity of small-scale explosive were characterized by T_{5s} and T_{1000s} . The bigger of those values, the lower of the thermal sensitivity.

$$\text{PBX-6: } T_{5s}=330^{\circ}\text{C} \quad T_{1000s}=255^{\circ}\text{C}$$



3.2 Critical temperatures and delay times of thermal explosion

□ Unlimited state

Table 1 Thermal explosion testing results of PBX-6 explosive cylinder

size	$T_a / ^\circ\text{C}$	$\Delta T / ^\circ\text{C}$	t / s	phenomena	$T_m / ^\circ\text{C}$
$\Phi 10\text{mm} \times 10\text{mm}$	212.0	11.2	13860	TE	210.0
	208.0	8.9	36000	TD	
$\Phi 20\text{mm} \times 20\text{mm}$	200.5	7.6	31200	TE	200.2
	199.9	7.0	36000	TD	
$\Phi 30\text{mm} \times 30\text{mm}$	198.0	7.9	29640	TE	197.5
	197.0	8.0	36000	TD	



The relationship of the critical parameter δ , the radius r and the critical temperature T_m can be expressed as

$$\ln\left(\frac{\delta T_m^2}{r^2}\right) = 162.34 - \left(\frac{115692}{T_m}\right)$$

$\Phi 40\text{mm} \times 40\text{mm}$
 $T_m = 194.6^\circ\text{C}$

The experiential relationship between the delay time t of thermal explosion and the environment temperature T_a is as follows.

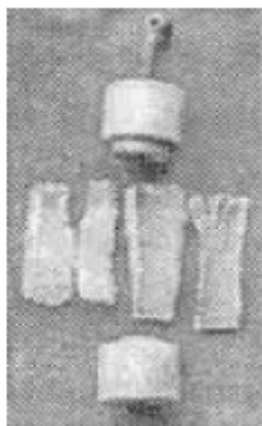
$$\ln t = C_2 + \frac{E}{RT_a}$$

$T_a > T_m \rightarrow \text{calculation } t$



Table 2 ODTX results of PBX-6 explosive cylinder

No.	$T_a / ^\circ\text{C}$	t / s	phenomena	grades	$T_m / ^\circ\text{C}$
PBX-6-3 [#]	194	14940	TE	high level reaction	189.5
PBX-6-4 [#]	192	15420	TE	high level reaction	
PBX-6-5 [#]	187	36000	TD	no reaction	
PBX-6-6 [#]	179	36000	TD	no reaction	



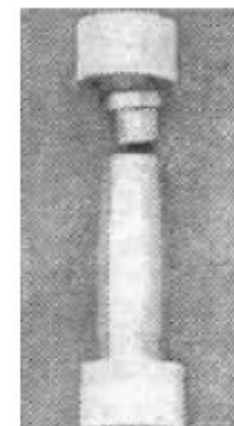
PBX-6-3[#]



PBX-6-4[#]



PBX-6-5[#]



PBX-6-6[#]

Fig.9 Deformation degree of tube contained sample



□ Constraint effect

Unlimited
One $\Phi 30 \times 30 \text{ mm}$
 $T_m = 197.5 \text{ }^\circ\text{C}$

$\Delta \Phi = -17.3 \text{ mm}$
 $\Delta T_m = -8 \text{ }^\circ\text{C}$

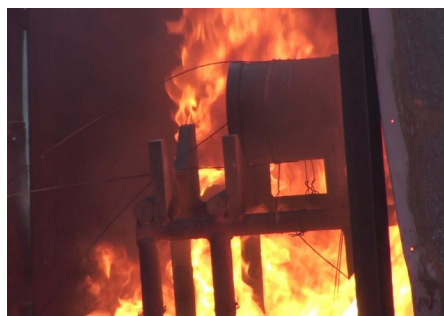
Limited
two $\Phi 12.7 \times 25.4 \text{ mm}$
 $T_m = 189.5 \text{ }^\circ\text{C}$

Because the explosive cylinders are confined, product of thermal decomposition is not easy to come out and the heat is not easy to convey to environment, and make it easier to reach the critical condition of thermal explosion comparing to the unlimited one.



3.3 Time and temperature of deflagration for cook-off test

□ Bonfire heating



bonfire



thermal decomposition

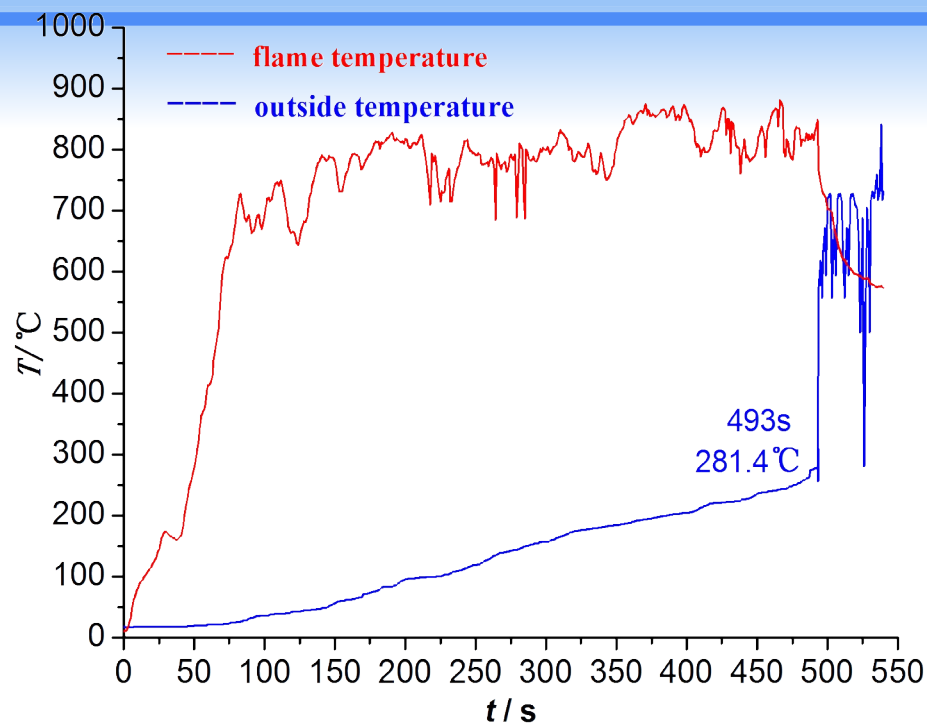


combustion



explosion

Fig.10 photographs of DV kinescope in fast cook-off test



HS-2# sample (65°C, 180d)



HS-1#



HS-2#



HS-3#

Fig.11 Temperature curves of explosive components measured in fast cook-off test

Fig.12 Photographs of scrap in fast cook-off test for PBX-6 explosive component

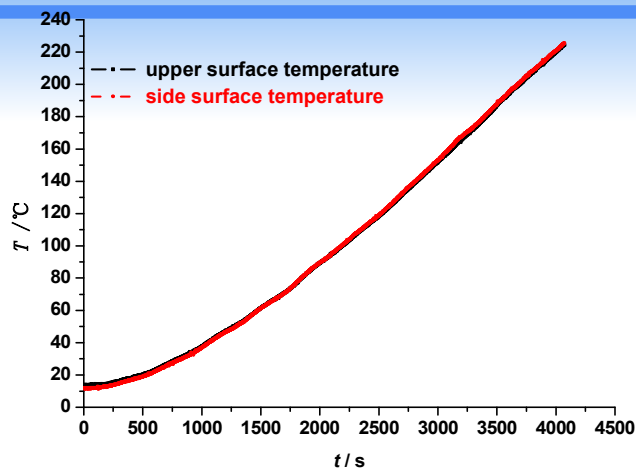


Table 3 Results of fast cook-off test for PBX-6 explosive components

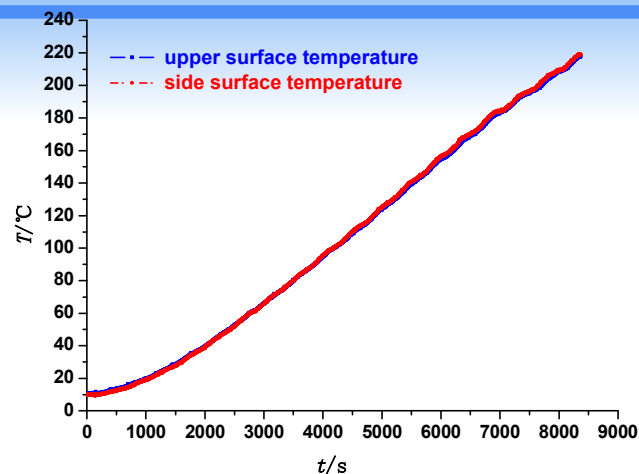
No.	condition of aging	ρ /(g·cm ⁻³)	deflagration time / s	deflagration temperature/°C	grade
HS-1 [#]	unaging	1.843	519	311.0	deflagration
HS-2 [#]	65°C, 180d	1.838	493	281.4	
HS-3 [#]	65°C, 365d	1.836	477	269.5	

The deflagration time was shortened, and the deflagration temperature was lowered with increasing of the aging time.

□ Slow heating



(a) 5°C/min



(b) 2°C/min

Fig.13 Change curves of surface temperature for the explosive spheres



MK-1# (5°C·min⁻¹)



MK-2# (2°C·min⁻¹)

Fig.14 Photographs of scrap in slow cook-off test of explosive components



Table 4 Results of slow cook-off test for PBX-6 explosive components

No.	heating rates $/(^{\circ}\text{C}\cdot\text{min}^{-1})$	deflagration time /s	deflagration temperature $/^{\circ}\text{C}$	shock wave overpressure /kPa	grade
MK-1 [#]	5	4074	224.9	21.8	deflagration
MK-2 [#]	2	8373	218.5	-	reaction

The deflagration time was shortened, and the deflagration temperature was increased with increasing of the heating rate.



(1) The methods of explosion point test of small scale explosive, thermal explosion test of explosive cylinder, and cook-off test of explosive spheres have been established.

(2) The thermal sensitivity and safety for PBX-6 explosive samples of different scales are synthetically evaluated by analyzing the response characteristics at various thermal stimulus.



(1) The cook-off test of specimens under conditions of different accelerated aging and long-term stored will be developed.

(2) The numerical simulation will be carried out. Combining testing and numerical results, the effects of aging on thermal safety of explosive components will be investigated.



Thank you